

Lecture 17: Type II Superconductors

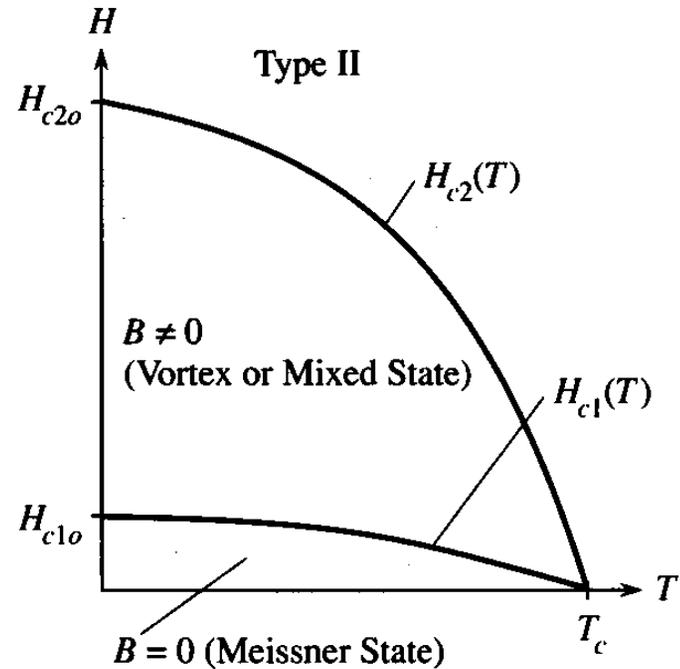
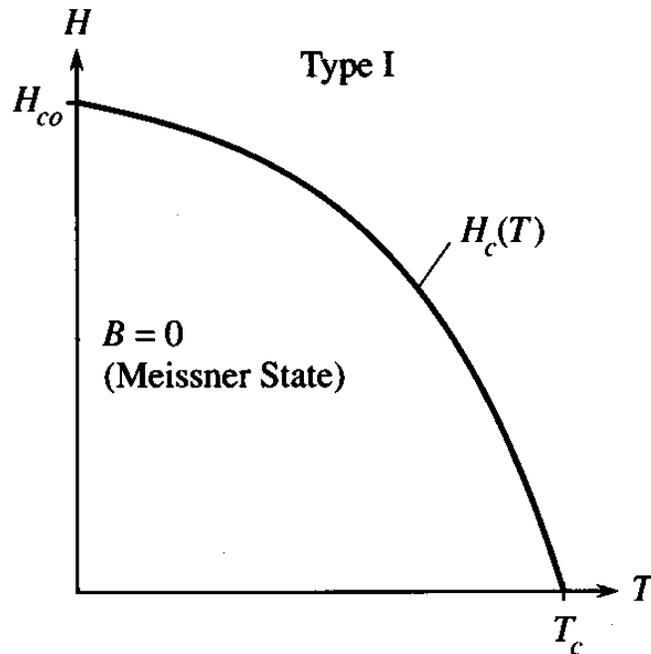
Outline

- 1. A Superconducting Vortex**
- 2. Vortex Fields and Currents**
- 3. General Thermodynamic Concepts**
 - **First and Second Law**
 - **Entropy**
 - **Gibbs Free Energy (and co-energy)**
- 4. Equilibrium Phase diagrams**
- 5. Critical Fields**

October 30, 2003



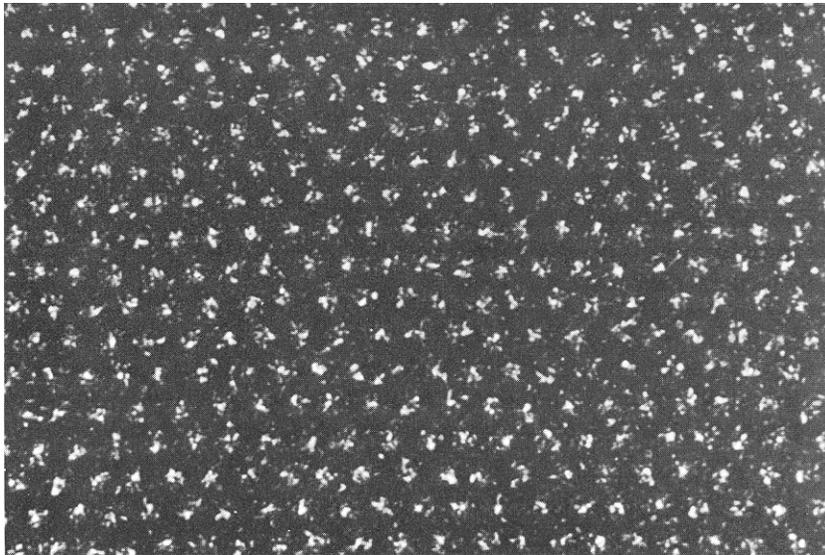
Fluxoid Quantization and Type II Superconductors



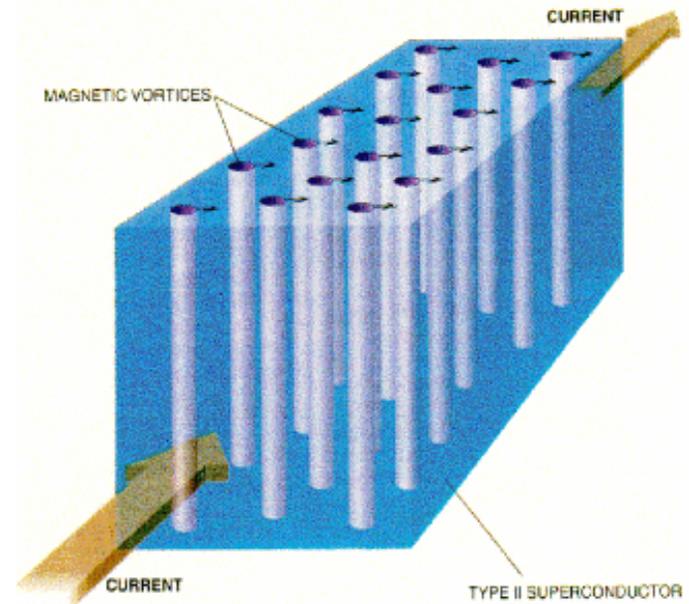
The Vortex State

$$\langle B \rangle = n_V \Phi_V$$

n_V is the areal density of vortices, the number per unit area.



Top view of Bitter decoration experiment on YBCO



Quantized Vortices

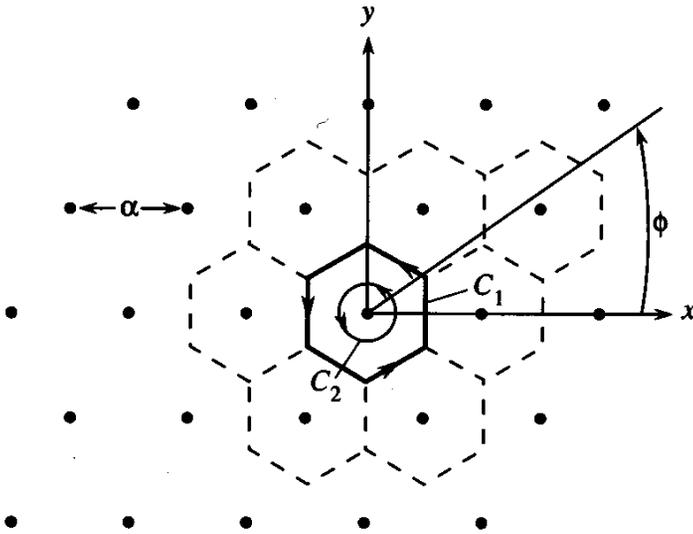
Fluxoid Quantization along C_1

$$n\Phi_0 = \oint_{C_1} \mu_0 \lambda^2 \mathbf{J}_S \cdot d\mathbf{l} + \int_{S_1} \mathbf{B} \cdot d\mathbf{s}$$

But along the hexagonal path C_1 \mathbf{B} is a minimum, so that \mathbf{J} vanishes along this path.

$$\text{Therefore, } n\Phi_0 = \int_{S_1} \mathbf{B} \cdot d\mathbf{s}$$

And experiments give $n = 1$, so each vortex has one flux quantum associated with it.



Along path C_2 ,
$$\Phi_0 = \oint_{C_2} \mu_0 \lambda^2 \mathbf{J}_S \cdot d\mathbf{l} + \int_{S_2} \mathbf{B} \cdot d\mathbf{s}$$

For small C_2 ,
$$\Phi_0 = \lim_{r \rightarrow 0} \oint_{C_2} \mu_0 \lambda^2 \mathbf{J}_S \cdot d\mathbf{l} \implies \lim_{r \rightarrow 0} \mathbf{J}_S = \frac{\Phi_0}{2\pi\mu_0\lambda^2} \frac{1}{r} \mathbf{i}_\phi$$

Normal Core of the Vortex

The current density $\lim_{r \rightarrow 0} \mathbf{J}_s = \frac{\Phi_0}{2\pi\mu_0\lambda^2} \frac{1}{r} \mathbf{i}_\phi$ diverges near the vortex center,

Which would mean that the kinetic energy of the superelectrons would also diverge. So to prevent this, below some core radius ξ the electrons become normal. This happens when the increase in kinetic energy is of the order of the gap energy. The maximum current density is then

$$\mathbf{J}_s^{\max} = \frac{\Phi_0}{2\pi\mu_0\lambda^2} \frac{1}{\xi} \mathbf{i}_\phi \quad \longrightarrow \quad \mathbf{v}_s^{\max} = \frac{\hbar}{m^*} \frac{1}{\xi} \mathbf{i}_\phi$$

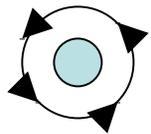
In the absence of any current flux, the superelectrons have zero net velocity but have a speed of the fermi velocity, v_F . Hence the kinetic energy with currents is

$$\mathcal{E}_{\text{kin}}^0 = \frac{1}{2} m^* v_F^2 = \frac{1}{2} m^* (v_{F,x}^2 + v_{F,y}^2 + v_{F,z}^2)$$



Coherence Length \boxtimes

The energy of a superelectron at the core is



$$\mathcal{E}_{\text{kin}}^1 = \frac{1}{2} m^* \left[v_{F,x}^2 + \left(v_{F,y} + v_{s,\phi}^{\text{max}} \right)^2 + v_{F,z}^2 \right]$$

The difference in energy, is to first order in the change in velocity,

$$\delta \mathcal{E} \approx m^* v_{F,y} v_{s,\phi}^{\text{max}} \approx \Delta$$

With $v_s^{\text{max}} = \frac{\hbar}{m^*} \frac{1}{\xi} \mathbf{i}_\phi$ this gives $\xi \approx \frac{\hbar v_F}{2\Delta}$

The full BCS theory gives the *coherence length* as $\xi_0 = \frac{\hbar v_F}{\pi \Delta_0}$

Therefore the maximum current density, known as the *depairing current density*, is

$$J_{\text{depair}} \approx \frac{\Phi_0}{2\pi \mu_0 \lambda^2 \xi}$$



Temperature Dependence

Both the coherence length and the penetration depth diverge at T_c

$$\lim_{T \rightarrow T_c} \xi(T) = \frac{\xi(0)}{\sqrt{1 - (T/T_c)}} \quad \lim_{T \rightarrow T_c} \lambda(T) = \frac{\lambda(0)}{\sqrt{1 - (T/T_c)}}$$

But their ratio, the Ginzburg-Landau parameter is independent of temperature near T_c

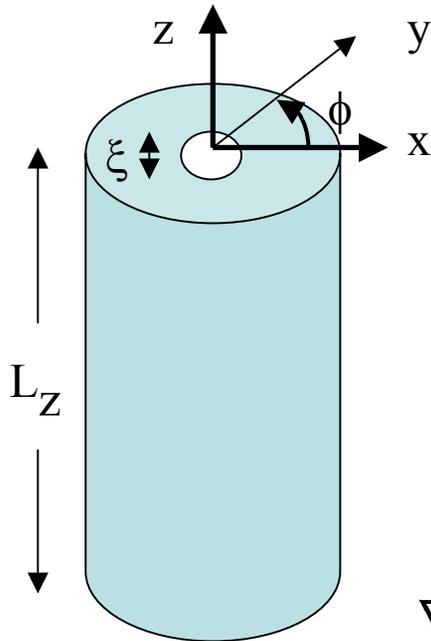
$$\kappa \equiv \frac{\lambda}{\xi}$$

$\kappa < 1/\sqrt{2}$ Type I superconductor Al, Nb

$\kappa > 1/\sqrt{2}$ Type II superconductor Nb, Most magnet materials $\kappa \gg 1$



Vortex in a Cylinder



London's Equations hold in the superconductor

$$\nabla \times (\Lambda \mathbf{J}_S) = -\mathbf{B}$$

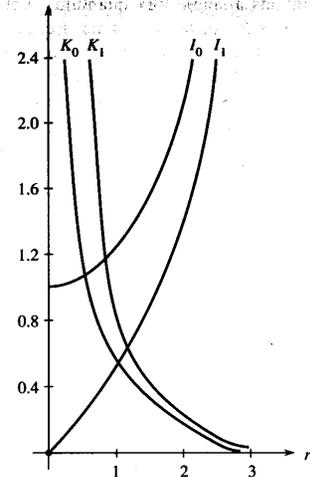
With Ampere's Law gives

$$\nabla^2 \mathbf{B}(\mathbf{r}) - \frac{1}{\lambda^2} \mathbf{B}(\mathbf{r}) = 0 \quad \text{for } r \geq \xi$$

Because \mathbf{B} is in the z-direction, this becomes a scalar Helmholtz Equation

$$\nabla^2 B_z - \frac{1}{\lambda^2} B_z = 0 \quad \text{for } r \geq \xi$$

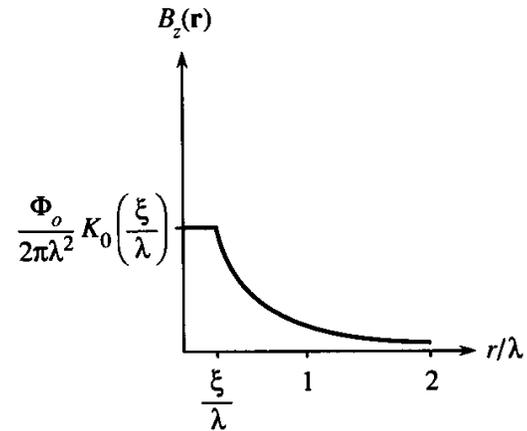
$$B_z(r, \phi) = \sum_{m=0}^{\infty} K_m \left(\frac{r}{\lambda}\right) (C_m \cos m\phi + C'_m \sin m\phi) + \sum_{m=0}^{\infty} I_m \left(\frac{r}{\lambda}\right) (D_m \cos m\phi + D'_m \sin m\phi)$$



Vortex in a cylinder

Which as a solution for an azimuthally symmetric field

$$B_z(r) = \begin{cases} C_0 K_0 \left(\frac{r}{\lambda} \right) & \text{for } r \geq \xi \\ C_0 K_0 \left(\frac{\xi}{\lambda} \right) & \text{for } r < \xi \end{cases}$$



C_0 is found from flux quantization around the core,

$$C_0 = \frac{\Phi_0}{2\pi\lambda^2} \left[\frac{1}{2} \frac{\xi^2}{\lambda^2} K_0 \left(\frac{\xi}{\lambda} \right) + \frac{\xi}{\lambda} K_1 \left(\frac{\xi}{\lambda} \right) \right]^{-1}$$

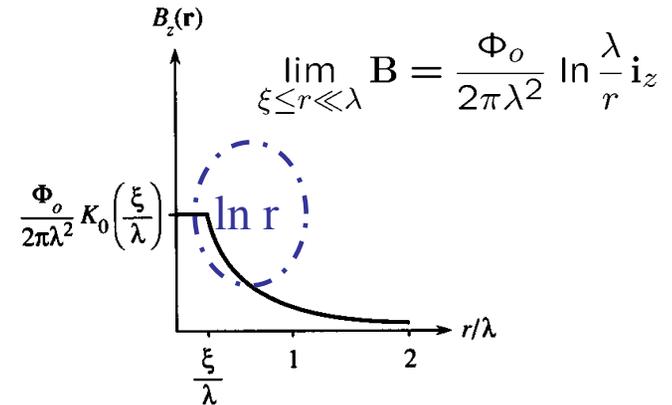
Which for $\kappa \gg 1$

$$C_0 = \frac{\Phi_0}{2\pi\lambda^2}$$

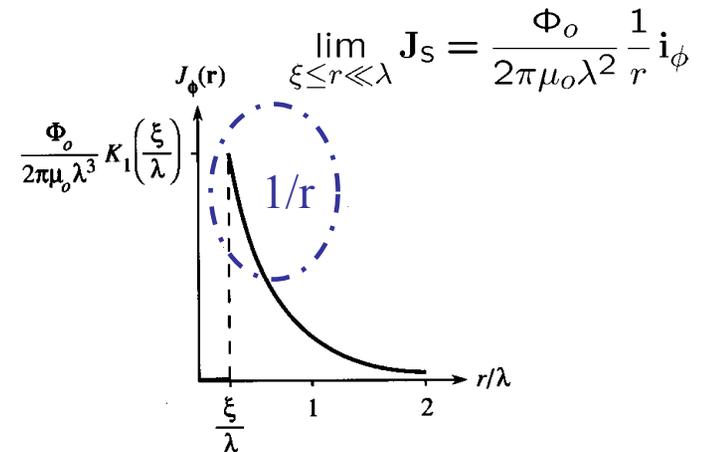


Vortex in a cylinder $\kappa \gg 1$

$$\mathbf{B}(\mathbf{r}) = \begin{cases} \frac{\Phi_0}{2\pi\lambda^2} K_0\left(\frac{r}{\lambda}\right) \mathbf{i}_z & \text{for } r \geq \xi \\ \frac{\Phi_0}{2\pi\lambda^2} K_0\left(\frac{\xi}{\lambda}\right) \mathbf{i}_z & \text{for } r < \xi \end{cases}$$



$$\mathbf{J}_S(\mathbf{r}) = \begin{cases} \frac{\Phi_0}{2\pi\mu_0\lambda^3} K_1\left(\frac{r}{\lambda}\right) \mathbf{i}_\phi & \text{for } r \geq \xi \\ 0 & \text{for } r < \xi \end{cases}$$



Energy of a single Vortex

The Electromagnetic energy in the superconducting region for a vortex is

$$W_s = \frac{1}{2\mu_0} \int_{V_s} [\mathbf{B}^2 + \mu_0 \mathbf{J}_s \cdot (\nabla \mathbf{J}_s)] dv$$

This gives the *energy per unit length* of the vortex as

$$\mathcal{E}_V = \frac{\Phi_0^2}{4\pi\mu_0\lambda^2} K_0\left(\frac{\xi}{\lambda}\right)$$

In the high κ limit this is

$$\lim_{\lambda \gg \xi} \mathcal{E}_V = \frac{\Phi_0^2}{4\pi\mu_0\lambda^2} \ln\left(\frac{\lambda}{\xi}\right)$$



Modified London Equation $\kappa \gg \lambda/\xi$

Given that one is most concerned with the high κ limit, one approximates the core of the vortex ξ as a delta function which satisfies the fluxoid quantization condition. This is known as the *Modified London Equation*:

$$\nabla \times (\Lambda \mathbf{J}_s) + \mathbf{B} = \mathbf{V}(\mathbf{r})$$

The vorticity is given by delta function along the direction of the core of the vortex and the strength of the vortex is Φ_0

For a single vortex along the z-axis:

$$\mathbf{V}(\mathbf{r}) = \Phi_0 \delta_2(\mathbf{r}) \mathbf{i}_z$$

For multiple vortices

$$\mathbf{V}(\mathbf{r}) = \sum_p \Phi_0 \delta_2(\mathbf{r} - \mathbf{r}_p) \mathbf{i}_z$$



General Thermodynamic Concepts

First Law of Thermodynamics: *conservation of energy*

$$\underbrace{dU}_{\text{Internal energy}} = \underbrace{dQ}_{\text{Heat in}} + \underbrace{dW}_{\text{E\&M energy stored}} - \underbrace{f_{\eta}d\eta}_{\text{work done by the system}}$$



W: Electromagnetic Energy

Normal region of Volume V_n

$$W_n = \int_{V_n} \frac{1}{2\mu_0} \mathbf{B}^2 dv$$

Superconducting region of Volume V_s

$$W_s = \frac{1}{2\mu_0} \int_{V_s} [\mathbf{B}^2 + \mu_0 \mathbf{J}_s \cdot (\nabla \mathbf{J}_s)] dv$$

In the absence of applied currents, in Method II, we have found that

$$dW = \int_V \mathbf{H} \cdot d\mathbf{B} dv$$

Moreover, for the simple geometries \mathbf{H} is a constant, proportional to the applied field. For a \mathbf{H} along a cylinder or for a slab, \mathbf{H} is just the applied field. Therefore,

$$dW = \mathbf{H} \cdot d \int_V \mathbf{B} dv$$



Thermodynamic Fields

$$dW = \mathbf{H} \cdot d \int_V \mathbf{B} dv$$

$$\vec{\mathcal{H}} \equiv \mathbf{H} \quad \text{thermodynamic magnetic field}$$

$$\vec{\mathcal{B}} = \frac{1}{V} \int_V \mathbf{B} \quad \text{thermodynamic flux density}$$

$$\vec{\mathcal{M}} = \frac{1}{\mu_0} \vec{\mathcal{B}} - \vec{\mathcal{H}} \quad \text{thermodynamic magnetization density}$$

Therefore, the thermodynamic energy stored can be written simply as

$$dW = V \vec{\mathcal{H}} \cdot d\vec{\mathcal{B}}$$



Entropy and the Second Law

The *entropy* S is defined in terms of the heat delivered to a system at a temperature T

$$dS \equiv \frac{dQ}{T}$$

Second Law of Thermodynamics:

For an isolated system in equilibrium $\Delta S = 0$

The **first law for thermodynamics** for a system in equilibrium can be written as

$$dU = T dS + V \vec{\mathcal{H}} \cdot d\vec{\mathcal{B}} - f_{\eta} d\eta$$

Then the internal energy is a function of S , B , and η

$$U = U(S, \mathcal{B}, \eta)$$

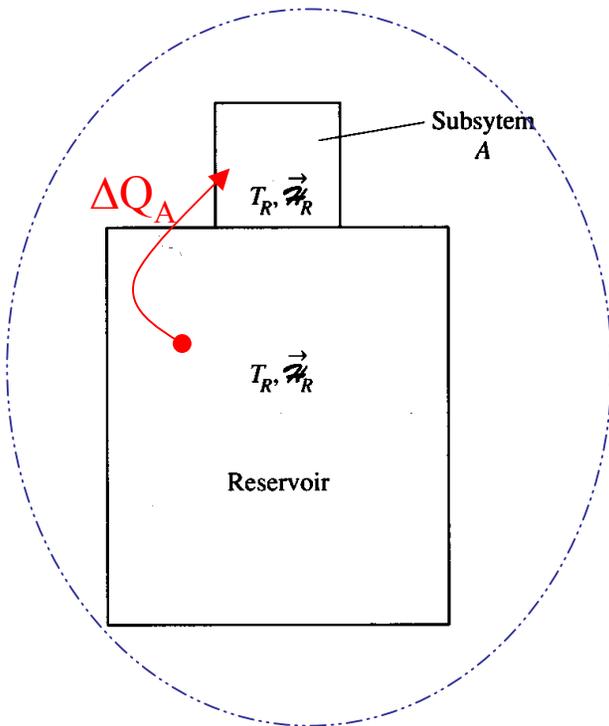
↕ ↕ ↕
 T, \mathcal{H}, f_{η} *Conjugate variables*



Concept of Reservoir and Subsystem

Because we have more control over the conjugate variables T, \mathcal{H}, f_η , we seek a rewrite the thermodynamics in terms of these controllable variables.

Isolated system = Subsystem + Reservoir



$$\Delta S_{\text{tot}} = \Delta S_A + \Delta S_R$$

The change in entropy of the reservoir is

$$\Delta S_R = \frac{\Delta Q_R}{T_R} = -\frac{\Delta Q_A}{T_R}$$

Therefore,
$$\Delta S_{\text{tot}} = \frac{T_R \Delta S_A - \Delta Q_A}{T_R}$$

$$\Delta S_{\text{tot}} = \frac{T_R \Delta S_A - \Delta U_A + V \vec{\mathcal{H}}_R \cdot \Delta \vec{\mathcal{B}} - f_\eta \Delta \eta}{T_R}$$

Gibbs Free Energy

The change total entropy is then

$$\Delta S_{\text{tot}} = \frac{-\Delta G_A - f_\eta \Delta \eta}{T_R} \geq 0$$

where the *Gibbs Free Energy* is defined by

$$G_A \equiv -T_R S_A + U_A - V \vec{\mathcal{H}}_R \cdot \vec{\mathcal{B}}$$

At equilibrium, the available work is just ΔG
(the energy that can be freed up to do work)
and the force is

Free Energy of subsystem
decreases

$$f_\eta = - \left. \frac{\partial G}{\partial \eta} \right|_{T, \vec{\mathcal{H}}}$$

$$\Delta G \leq 0$$



Gibbs Free Energy and Co-energy

The Gibbs free energy is

$$G = -TS + U - V\vec{\mathcal{H}} \cdot \vec{\mathcal{B}}$$

The differential of G is

$$dG = -T dS - S dT + dU - V d\vec{\mathcal{H}} \cdot \vec{\mathcal{B}} - V\vec{\mathcal{H}} \cdot d\vec{\mathcal{B}}$$

and with the use of the first law $dU = T dS + V\vec{\mathcal{H}} \cdot d\vec{\mathcal{B}} - f_\eta d\eta$

$$dG = -S dT - V \vec{\mathcal{B}} \cdot d\vec{\mathcal{H}} - f_\eta d\eta$$

Therefore, the Gibbs free energy is a function of T, \mathcal{H}, η

At constant temperature and no work, then $dG|_{T,\eta} = -d\tilde{W}$ the co-energy

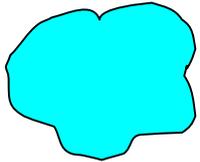
$$f_\eta = - \left. \frac{\partial G}{\partial \eta} \right|_{T,\vec{\mathcal{H}}} = \left. \frac{\partial \tilde{W}}{\partial \eta} \right|_{T,\vec{\mathcal{H}}} \quad \text{Note minus sign!}$$



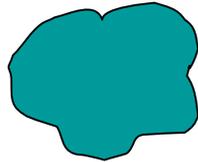
Gibbs Free Energy and Equilibrium

In Equilibrium $\Delta G = 0$

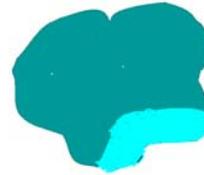
Consider the system made up of two phases 1 and 2



Phase 1, $G = G_1$



Phase 2, $G = G_2$



Mixed phase $G_{\text{tot}} = G_1 \frac{V_1}{V} + G_2 \frac{V_2}{V}$

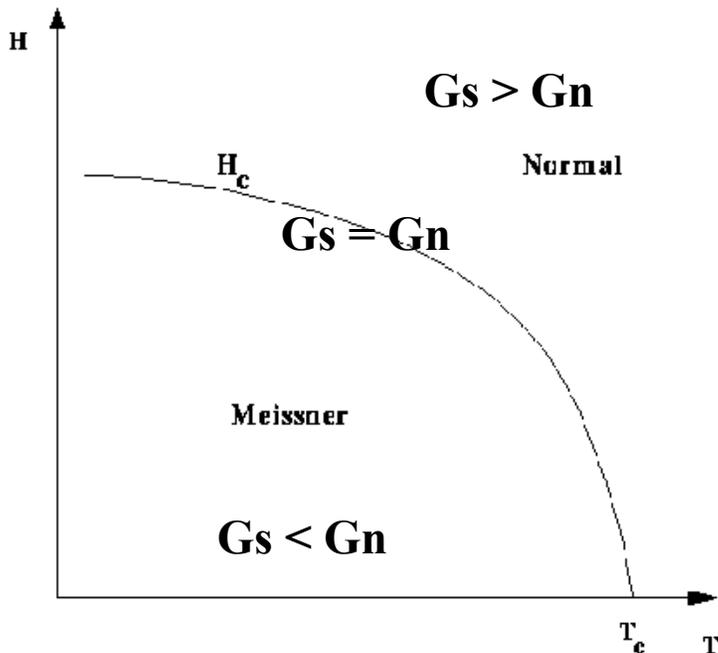
Therefore, $G_{\text{tot}} = (G_1 - G_2) \frac{V_1}{V} + G_2$ is minimized when $G_1 = G_2$

Two phases in equilibrium with each other have the same Gibbs Free Energy



Phase Diagram and Critical Field

$\Delta G < 0$ So that G is always minimized, the system goes to the state of lowest Gibbs Free Energy. At the phase boundary, $G_s = G_n$.



At zero magnetic field in the superconducting phase

$$G_s(\vec{H}, 0) < G_n(\vec{H}, 0)$$

for $T < T_c$

$$G_s(0, T) - G_n(0, T) \equiv \underbrace{-\frac{1}{2} \mu_0 H_c^2(T) V_s}_{\text{condensation energy}}$$

The *Thermodynamic Critical Field* $H_c(T)$ is experimentally of the form

$$H_c(T) \approx H_{c0} \left(1 - \left(\frac{T}{T_c} \right)^2 \right) \quad \text{for } T \leq T_c$$



Critical Field for Type I

Recall that $dG = -V \vec{B} \cdot d\vec{\mathcal{H}}$

In the bulk limit in the superconducting state $B = 0$ so that $dG_s = 0$

Likewise in the normal state $\vec{\mathcal{H}} = \mathbf{H}_{\text{app}}$ and $\vec{B} = \mu_0 \vec{\mathcal{H}}$ so that

$$dG_n = -V \mu_0 \vec{\mathcal{H}} \cdot d\vec{\mathcal{H}}$$

Hence, we can write $d(G_s(\vec{\mathcal{H}}, T) - G_n(\vec{\mathcal{H}}, T)) = V \mu_0 \vec{\mathcal{H}} \cdot d\vec{\mathcal{H}}$

Integration of the field from 0 to H gives

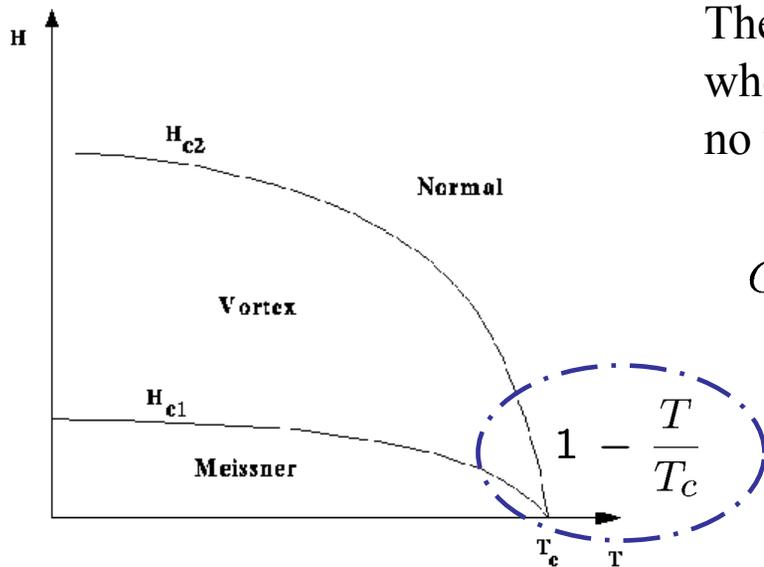
$$G_s(\vec{\mathcal{H}}, T) - G_n(\vec{\mathcal{H}}, T) = G_s(0, T) - G_n(0, T) + \frac{1}{2} V \mu_0 \vec{\mathcal{H}}^2$$

and thus

$$G_s(\mathcal{H}, T) - G_n(\mathcal{H}, T) = \frac{1}{2} \mu_0 (\mathcal{H}^2 - H_c^2) V$$



Critical Fields for Type II



The *lower critical field* H_{c1} is the phase boundary where equilibrium between having one vortex and no vortex in the superconducting state.

$$G_s^1(\vec{H}, T) = \underbrace{G_s^0(0, T)}_{G_s^0(0, H)} + \underbrace{W_s}_{\mathcal{E}_V L_z} - \underbrace{\vec{H} \cdot \int_{V_s} \mathbf{B} dv}_{\Phi_0 L_z}$$

Therefore

$$H_{c1} = \frac{\mathcal{E}_V}{\Phi_0} = \frac{\Phi_0}{4\pi\mu_0\lambda^2} \underbrace{K_0\left(\frac{\xi}{\lambda}\right)}_{\ln \lambda/\xi}$$

The *upper critical field* H_{c2} occurs when the flux density is such that the cores overlap:

$$H_{c2} = \frac{\Phi_0}{2\pi\mu_0\xi^2}$$

